

# Computational Techniques for the Analysis and Design of Dielectric-Loaded Plasmonic Circuitry

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T. V. Yioultsis, and E. E. Kriezis

## Outline

- Introduction
  - Single Interface and SPPs
  - The DLSPP Waveguide
  - DLSPP-Based Components
- Microdisk/ring Filters
  - Layout and Operating Principle
  - 3D-FEM Implementation Details
  - Small Radii
  - Large Radii
  - Thermally-Tunable Add-Drop Filters
- 2x2 MZI Switch
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  - Steady-State Response
  - Thermal Transient
  - Optical Transient
- Conclusions

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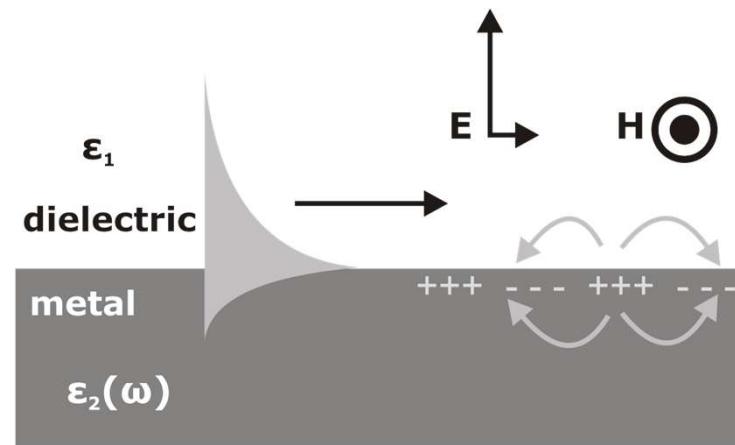
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## Introduction — Single Interface and SPPs

### Surface Plasmon Polaritons (SPPs):

Electromagnetic surface waves coherently coupled to free electron oscillations.

- Propagate along a metal-dielectric interface.
- Fields decay exponentially away from the interface.
- Exhibit propagation losses due to resistive damping in the metallic film.
- Trade-off between propagation losses and lateral confinement.



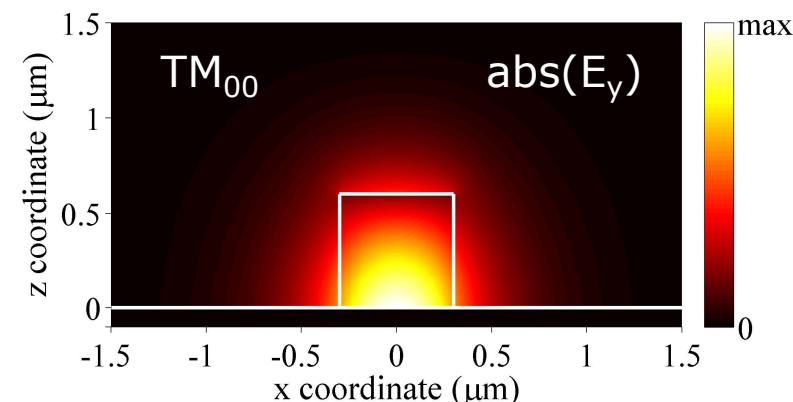
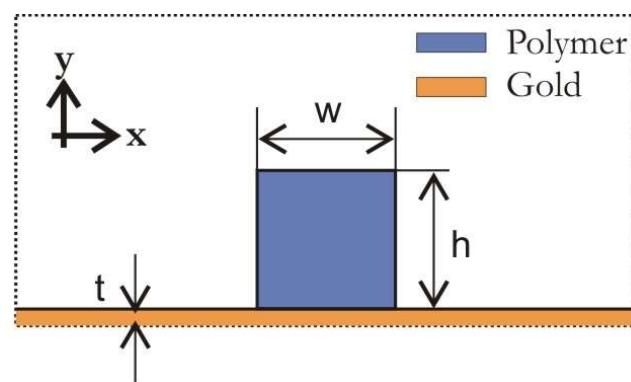
SPP at single metal-dielectric interface:  
An elementary plasmonic waveguide.

## Introduction — The DLSPP Waveguide

Dielectric-loaded surface plasmon polariton (DLSPP) waveguide:

- ✓ Technologically simple
- ✓ (2D) Sub-wavelength confinement and strong guiding properties.
- ✓ Relatively low propagation losses ( $L_{\text{prop}} \sim 45 \mu\text{m}$  for TM<sub>00</sub> mode)
- ✓ Readily accommodates diverse loadings → Dynamic components

T. Holmgaard, S.I. Bozhevolnyi, *Phys. Rev. B*, 75, 245405, 2006



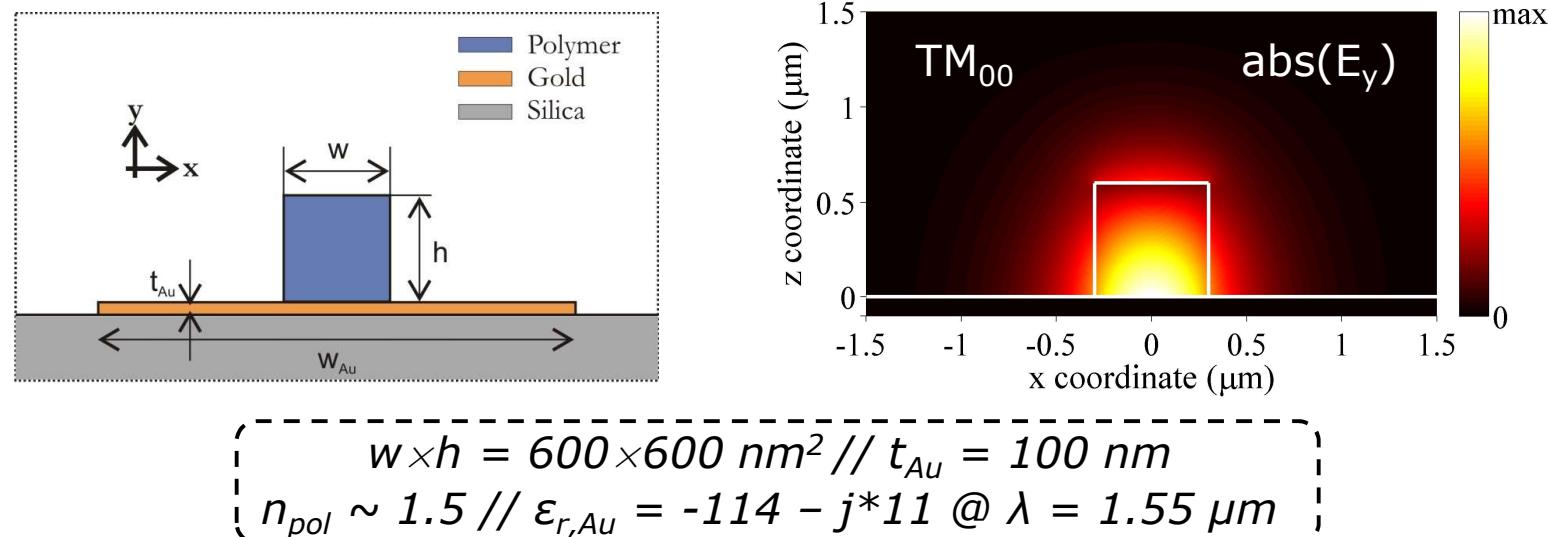
$$\boxed{\begin{aligned} w \times h &= 600 \times 600 \text{ nm}^2 // t_{Au} = 100 \text{ nm} \\ n_{pol} &\sim 1.5 // \epsilon_{r,Au} = -114 - j*11 @ \lambda = 1.55 \mu\text{m} \end{aligned}}$$

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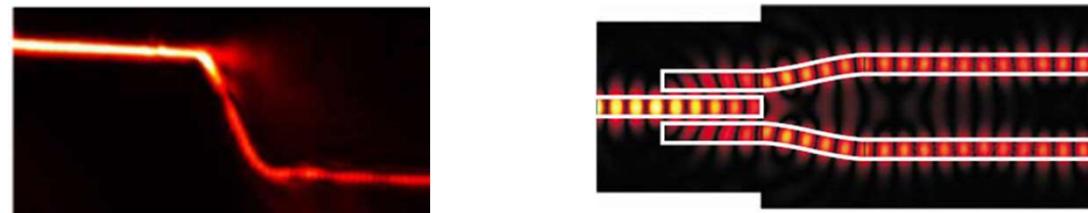
T. Holmgaard, S.I. Bozhevolnyi, *Phys. Rev. B*, 75, 245405, 2006



## Introduction — DLSPP-Based Components

### Passive components:

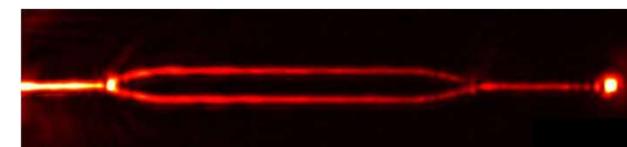
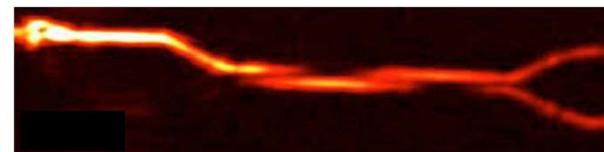
- ✓ Waveguide bends
- ✓ Coupled lines
- ✓ Splitters



A.V. Krasavin, A.V. Zayats, *Phys. Rev. B*, 78, 045425, 2008  
T. Holmgaard, et al., *Opt. Express*, 16, 13586, 2008

More recently, interest is focused on wavelength-selective components:

- ✓ Bragg reflectors
- ✓ Directional couplers
- ✓ MZIs
- ✓ Microring/disk resonator filters



T. Holmgaard, et al., *Appl. Phys. Lett.*, 94, 051111, 2009  
Z. Chen, et al., *Opt. Lett.*, 34, 310, 2009

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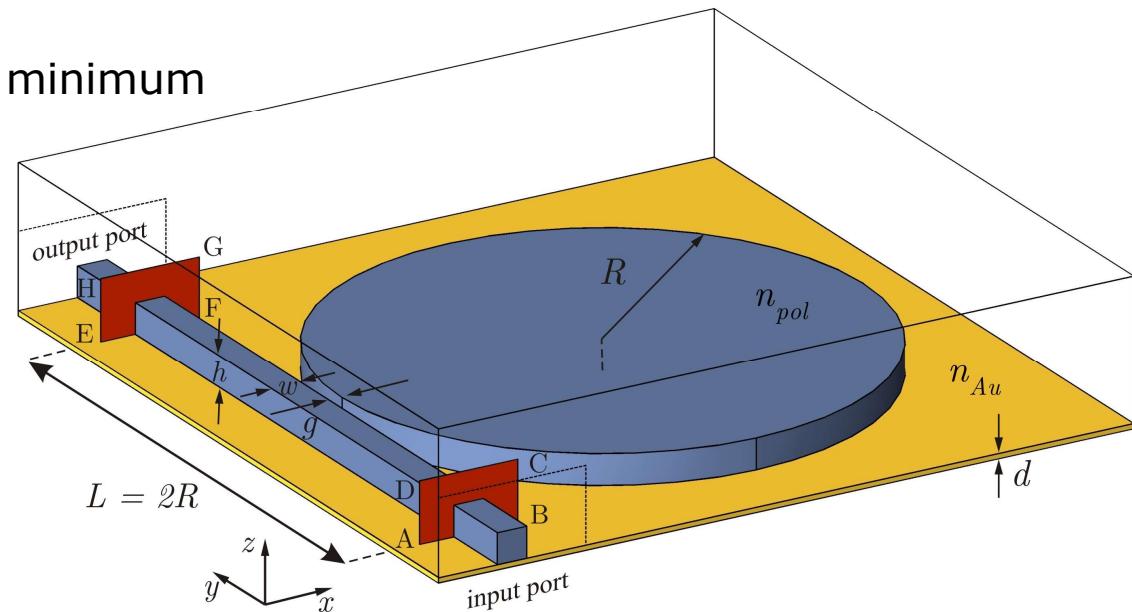
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## Microdisk/ring Filters – Layout and Operating Principle

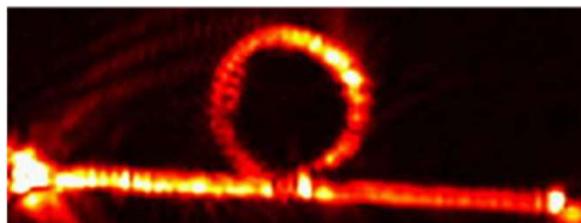
- ✓ Wavelength selective component
- ✓ Resonator coupled to bus w/g
- ✓ On resonance transmission is minimum
- ✓ Periodic response w.r.t.  $\lambda$
- ✓ Two loss mechanisms

### Crucial Parameters:

- Resonator-w/g gap  $g$   
(critical coupling - ER)
- Resonator radius  $R$   
(FSR, loss per circulation)



*Microring resonator filters have been experimentally and theoretically investigated.*

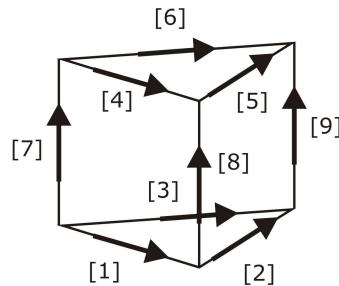


T. Holmgaard, et al., Opt. Express, 17, 2968, 2009  
O. Tsilipakos, et al., J. Appl. Phys., 106, 093109, 2009

## Microdisk/ring Filters – 3D-FEM Implementation Details

✓ 1<sup>st</sup> order triangular prisms

- 9 prism layers in total → 2(Au)+4(Pol.)+3(Air)



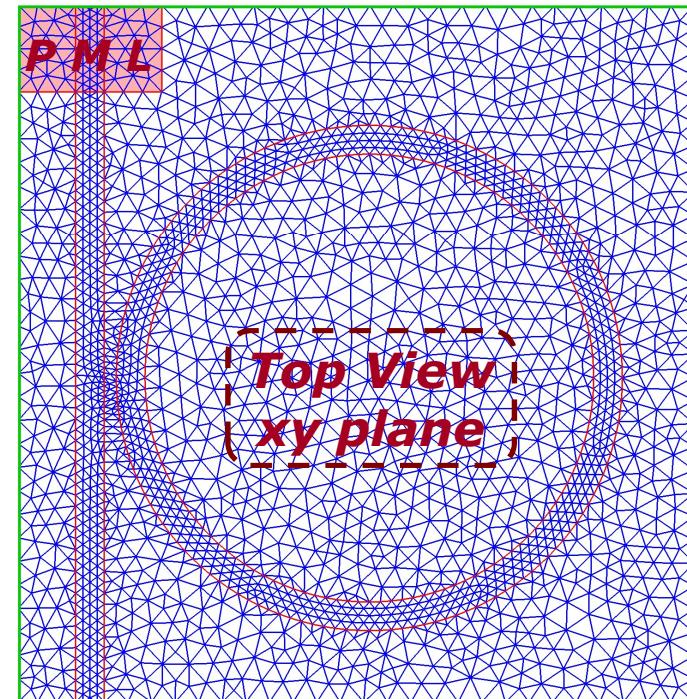
✓ 1<sup>st</sup> order absorbing boundary conditions (ABCs) on all sides and the top of the bounding box.

$$\hat{n} \times (\nabla \times \mathbf{E}) + jk_0 \hat{n} \times (\hat{n} \times \mathbf{E}) = 0$$

Modified for the I/O waveguide ports (hybrid mode)

Output:  $\hat{n} \times (\nabla \times \mathbf{E}) + j\beta \hat{n} \times (\hat{n} \times \mathbf{E}) = 0$

→  $j \frac{\omega \mu_0}{Z_w^{TM}(x, z)}$ , where  $Z_w^{TM}(x, z) = -\frac{E_z(x, z)}{H_x(x, z)}$



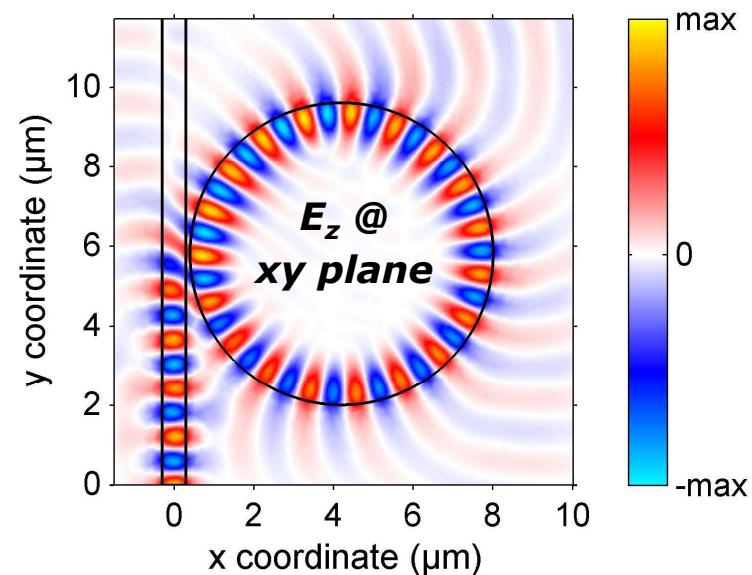
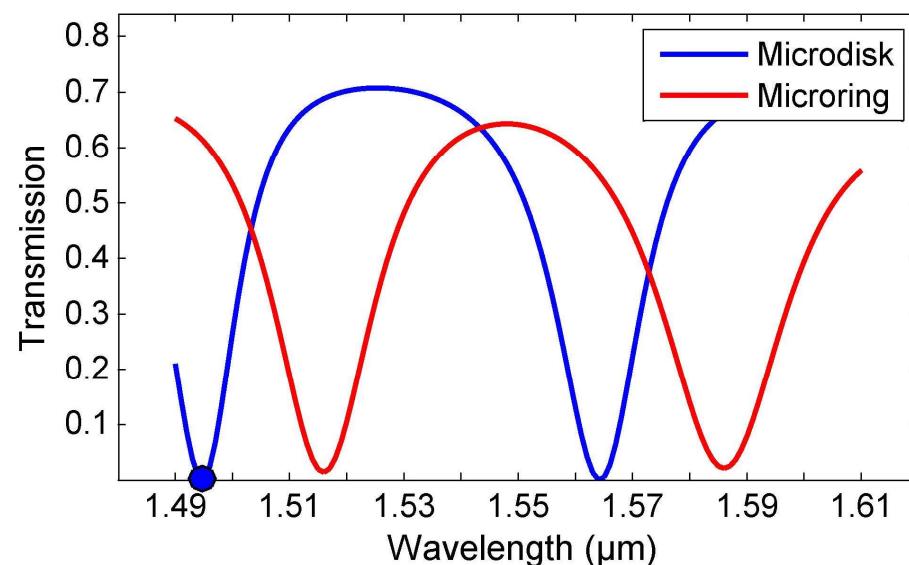
✓ Perfectly matched layer (PML) for the reflectionless termination of the bus w/g.

- Only **locally** employed. Global utilization → Increases DoFs & Degrades conditioning.

## Microdisk/ring Filters – Small Radii

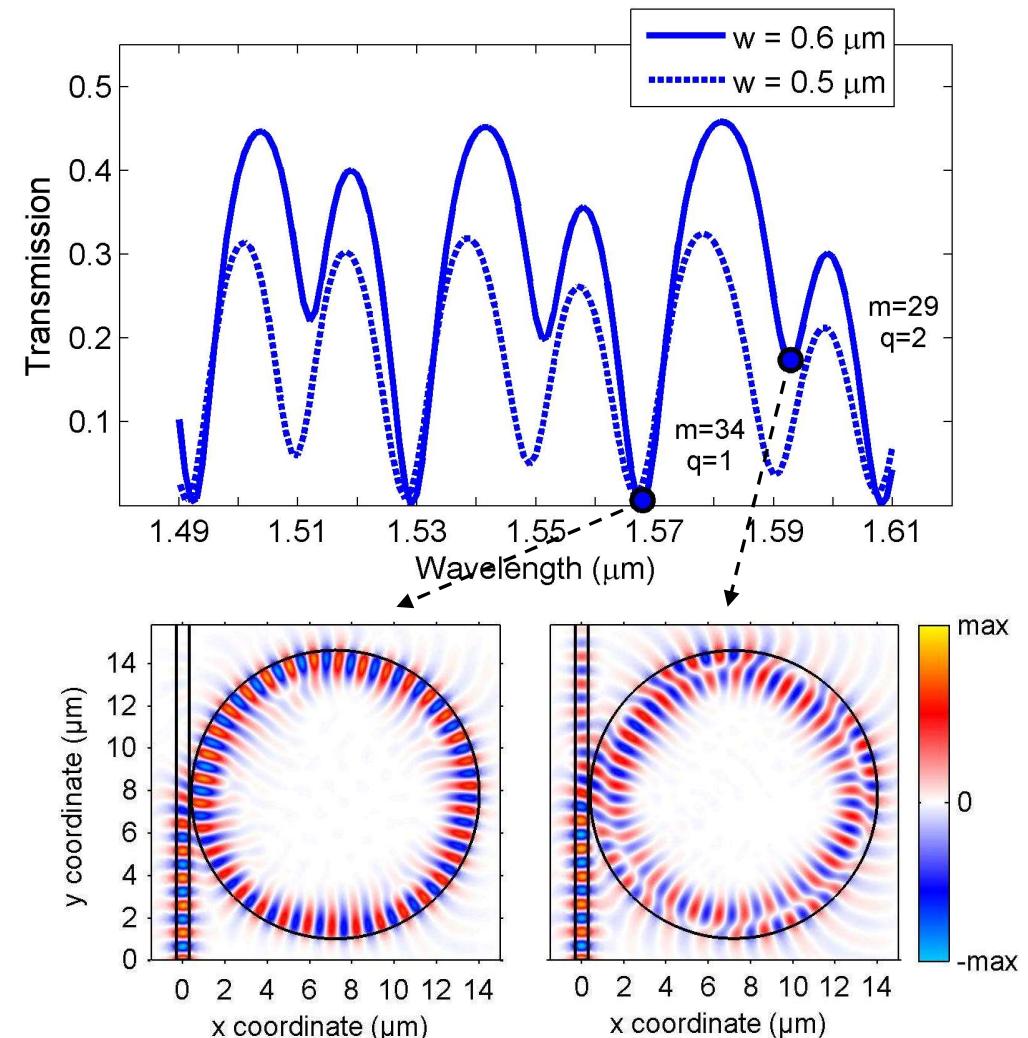
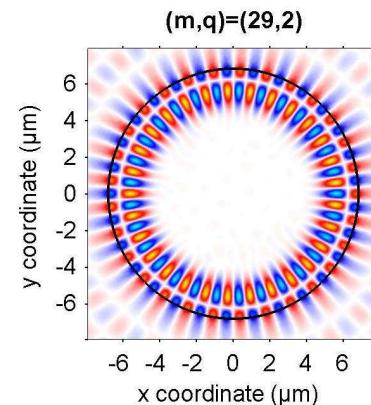
- Small radii → significant radiation losses (compared to resistive ones)
- Reduced radiation losses for the microdisk
  - Narrower minima linewidths
  - Eigenvalue simulations:  $Q_D \sim 200$  vs  $Q_R \sim 100$
  - Higher transmission maximum
- FSR  $\sim 70$  nm // ER  $> 15$  dB

$R = 3.8 \mu m$   
 $g = 0.1 \mu m$   
(critical coupling)



## Microdisk/ring Filters – Large Radii

- ✓  $R = 6.8 \mu\text{m}$ ,  $g = 0.1 \mu\text{m}$
- ✓ 2<sup>nd</sup> radial order modes ( $q=2$ )

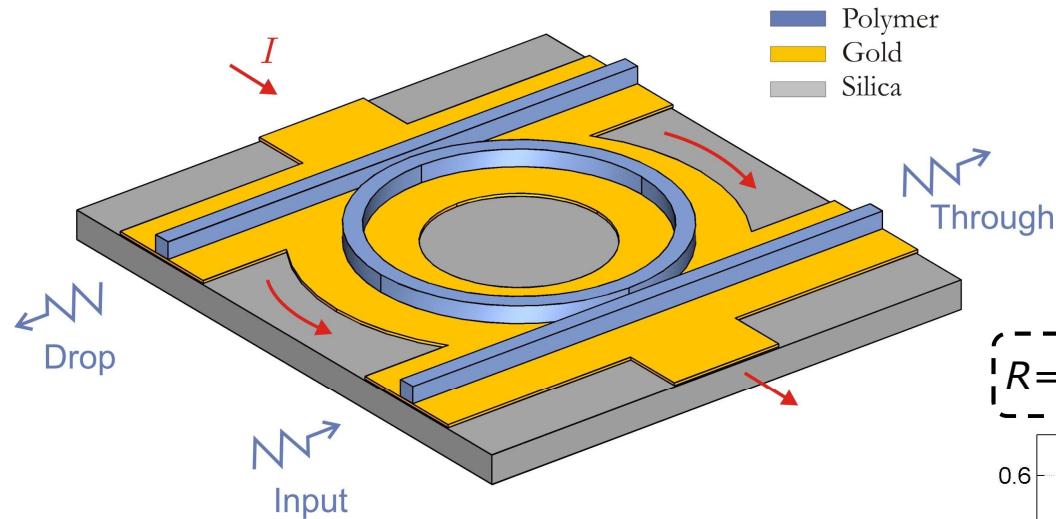


Excitation efficiency tuning:

- Waveguide width
- Disk radius

At  $\lambda=1.593 \mu\text{m}$  the  $E_z$  plot reveals a linear combination of modes (33,1) and (29,2)

## Microdisk/ring Filters – Thermally Tunable Add-Drop Filters

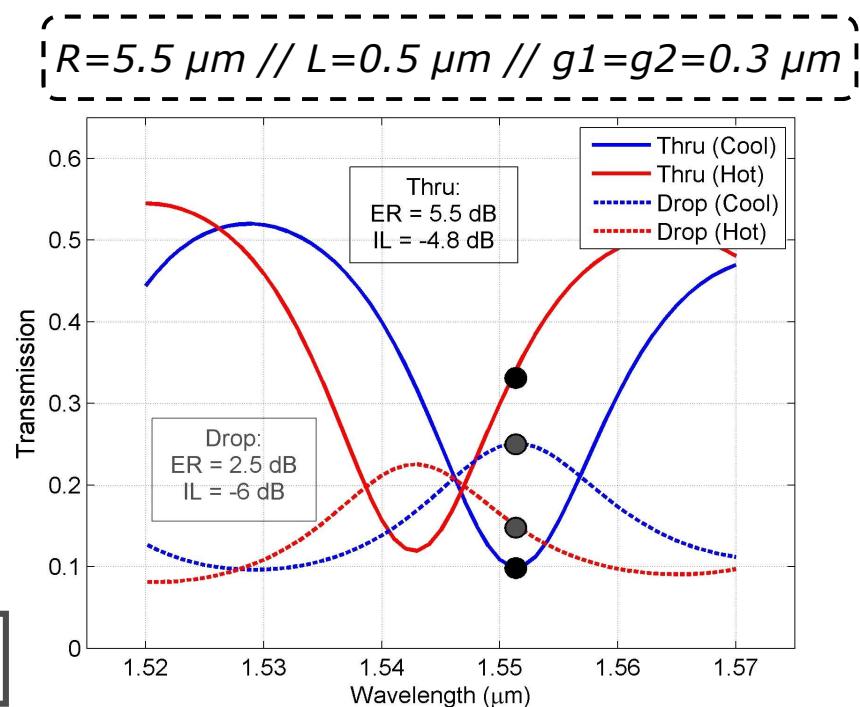


- Operating w/l @ maximum of drop
- $\sim 9$  nm shift ( $TOC \sim 10^{-4}$ ,  $\Delta T = 100$  K)
- Crosstalk  $\sim -4$  dB for both states
- $IL(\text{drop}) = -6$  dB
- $ER(\text{drop}) = 2.5$  dB

More on thermo-optic DLSPP-based components:

J. Gosciniak, et al., Opt. Express, 18, 1207, 2010  
 O. Tsilipakos, et al., J. Appl. Phys., 106, 093109, 2009

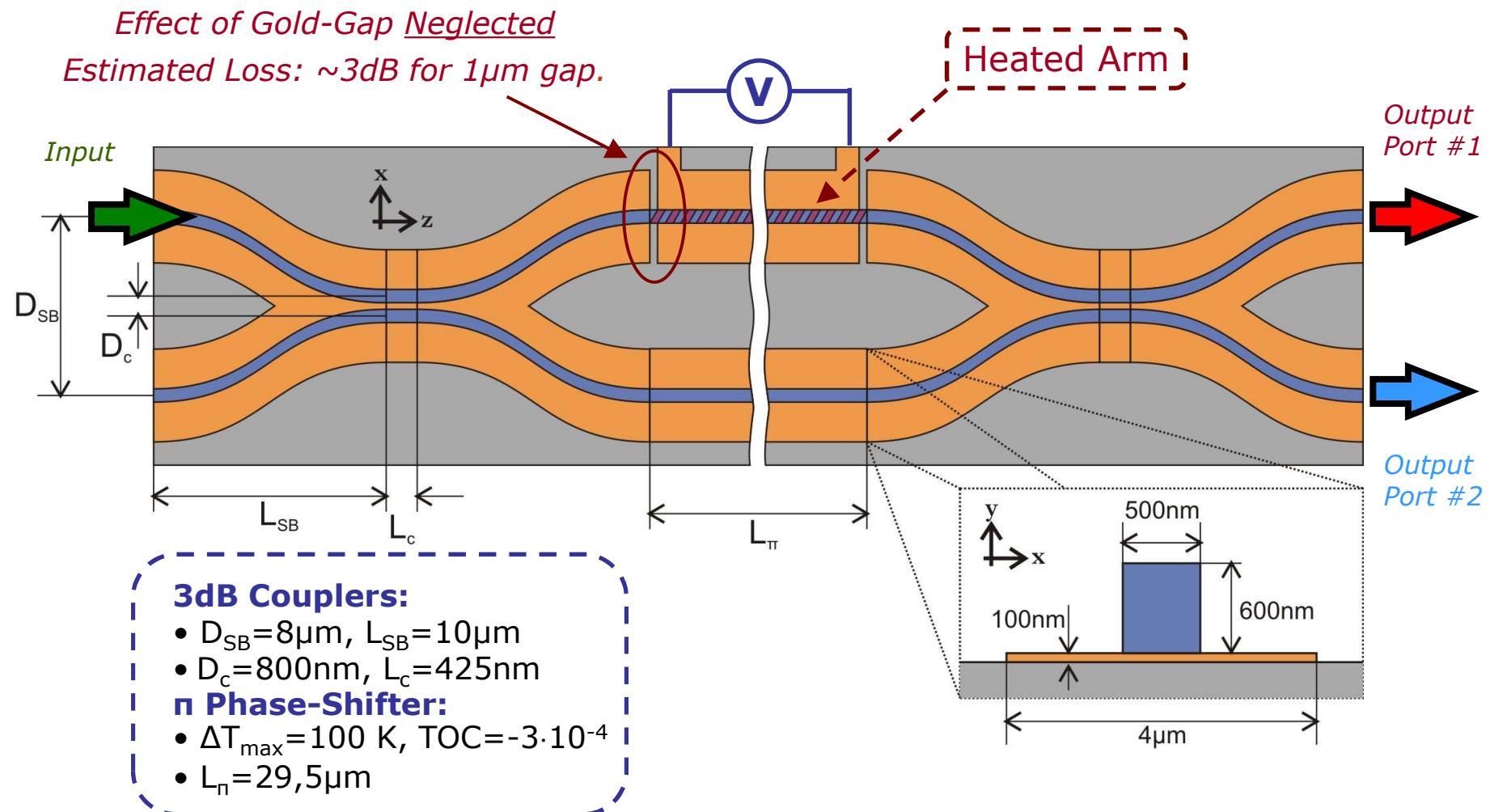
- ✓ Two bus waveguides
- ✓ Patterned metallic film
- ✓ Possibly racetrack shape
- ✓ SOI substrate



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## 2x2 MZI Switch – Layout and Operating Principle



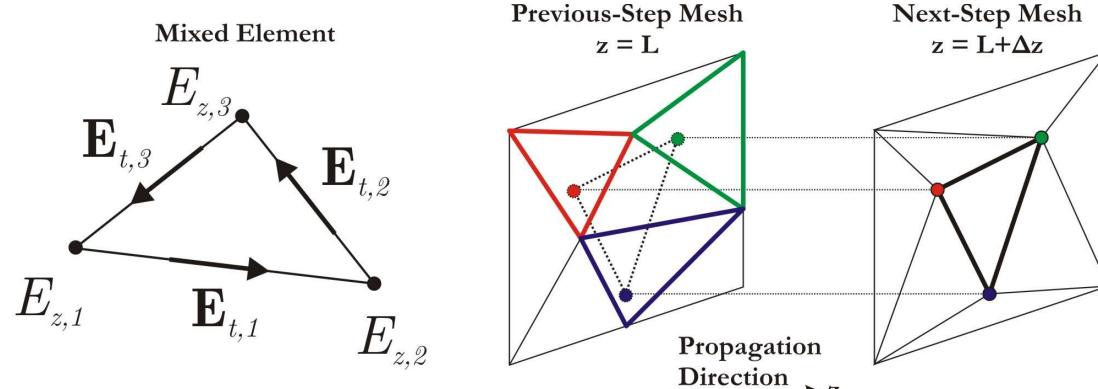
## 2x2 MZI Switch – 3D-BPM Implementation Details

### FD-BPM

- Dramatic discontinuities on interfaces w/ Au
- Grid w/ Collocated DoFs
  - *The continuity of  $E_n$  is falsely imposed*
  - *$\text{Im}\{n_{\text{eff}}\}$  is miscalculated*
- Yee grid gives fairly accurate results

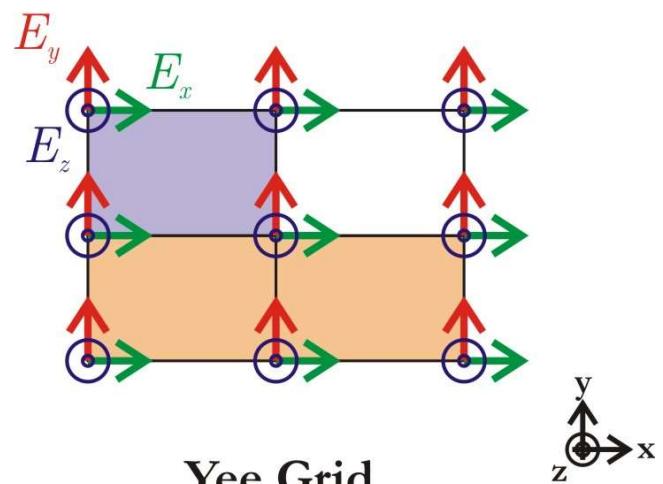
### FE-BPM

- Mixed elements: edge ( $\mathbf{E}_t$ ) + nodal ( $E_z$ )
- Effective index corrected (real and imag. part)
- Computational overhead for z-varying structures

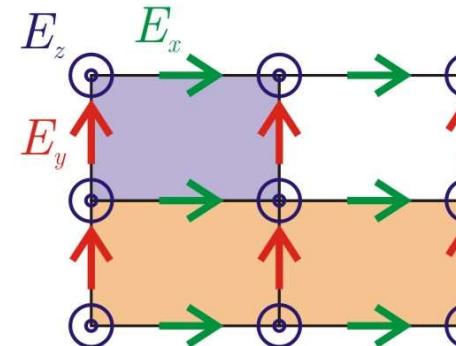


✓ The semi-vector TM BPM gives satisfactory results

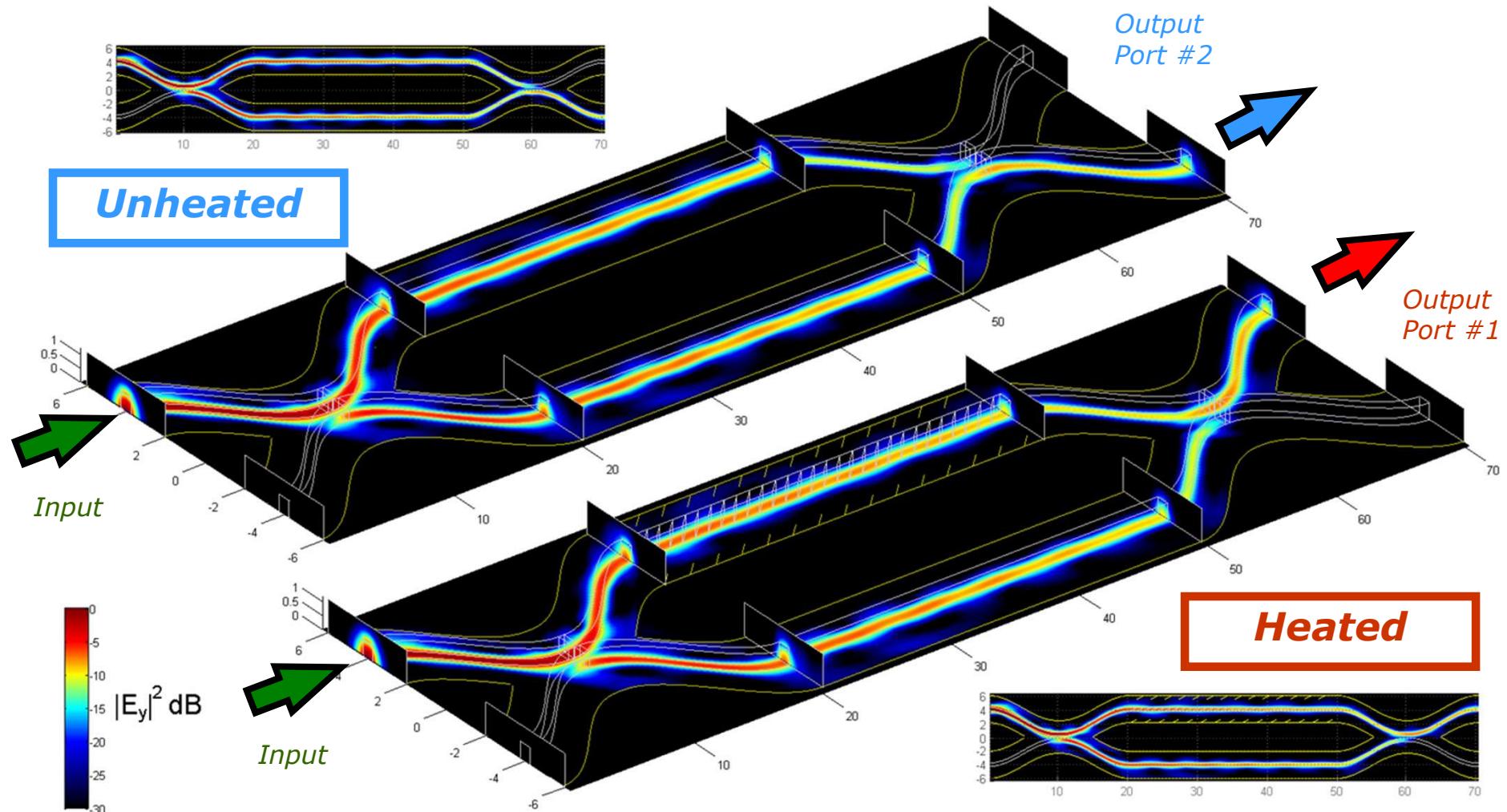
### Grid w/ Collocated DoFs



### Yee Grid



## 2x2 MZI Switch – Steady State Response



## 2x2 MZI Switch – Thermal Transient

✓  $V = 1.2 \text{ V} \rightarrow J = 100 \text{ GA/m}^2$

✓ Temperature distribution calculated through  
(time-stepping in increments of  $0.1 \mu\text{s}$  up to  $10 \mu\text{s}$ )

$$\rho C_p \frac{\partial T}{\partial t} + \nabla \cdot (-K \nabla T) = Q \equiv \frac{J^2}{\sigma}$$

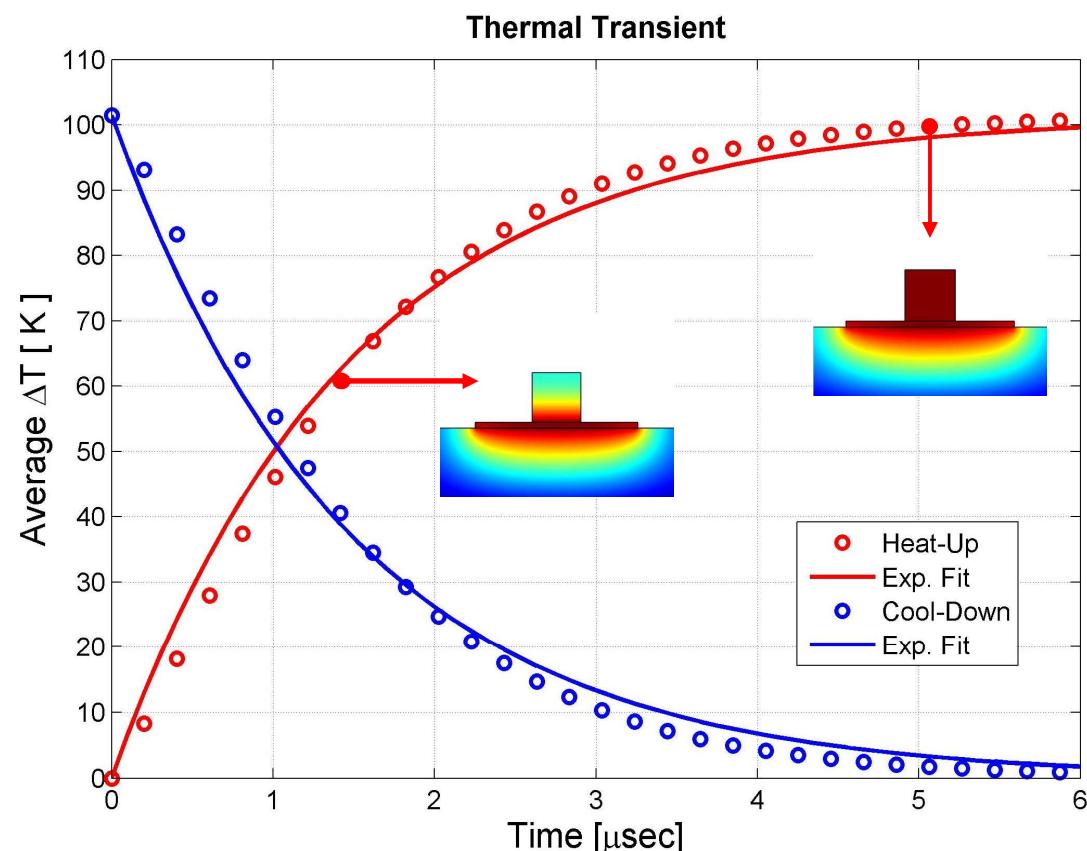
Exponential fits:

$$\Delta T_{av}(t) = \Delta T_{av}^\infty \left( 1 - e^{-t/\tau_{rise}} \right)$$

$$\Delta T_{av}(t) = \Delta T_{av}^\infty \left( e^{-t/\tau_{fall}} \right)$$

$$\tau_{rise} = \tau_{fall} = 1.5 \mu\text{s}$$

- $\Delta T$  is spatially constant in DL only in steady state
- Non-uniform distribution during transient



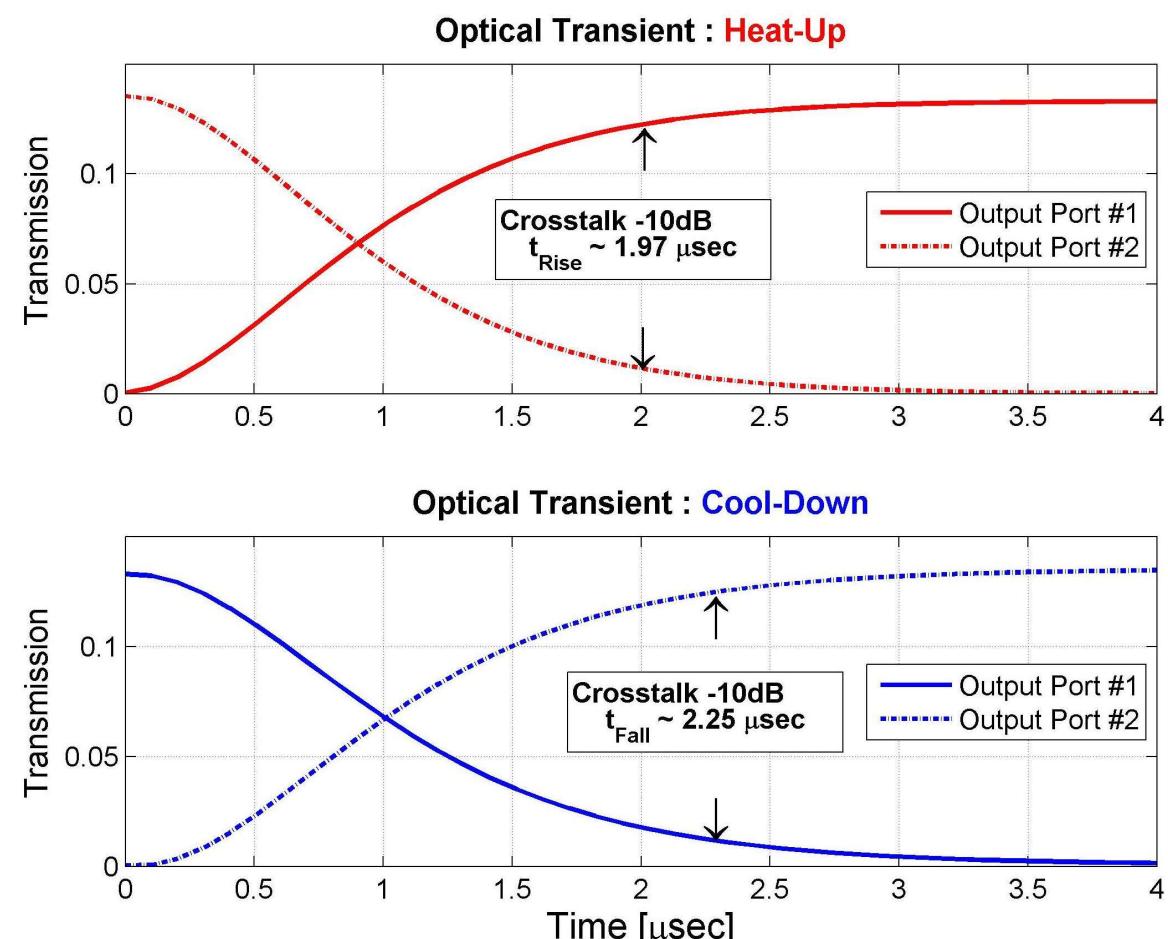
## 2x2 MZI Switch – Optical Transient

- **Switching Time: 1.97  $\mu$ s (Heat-Up) and 2.25  $\mu$ s (Cool-down)**

(Assuming -10 dB crosstalk between output ports)

**Insertion Loss:** ~9dB

- Propagation Losses (~ 0.1 dB/ $\mu$ m)
- S-Bend Losses (~ 1 dB per coupler)



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## Conclusions

- Thermally tunable DLSPP-based components
  - 3D-FEM for small resonant structures
  - 3D-BPM for large structures with clear propagation direction
- Other switching configurations possible
  - Directional coupler switch
  - MMI switch
- Polymers with higher TOC would be beneficial
- Other types of addressing for faster switching

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