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# Non-reciprocal Silicon Photonic Coupler Exploiting Graphene Saturable Absorption

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#### Introduction

Demand for on chip integrated optical isolators

- Magneto-optic components are bulky/expensive/hard to integrate.
- ✓ **Non-linear non-reciprocity** : Non-linearity + asymmetry breaks reciprocity.
  - Common implementation: Resonant components + Kerr effect.
    - **\*** Resonators: **high isolation** but **low bandwidth.**
- □ This work: Directional coupler + Saturable Absorption (SA).
  - The asymmetry is enhanced by the Exceptional Point (EP)

of the non-Hermitian (lossy) coupler.

- ✤ Non-linearity (SA) is provided by Graphene.
- $\checkmark$  Compatible **integration** with SOI platforms.
- ✓ Relaxed **bandwidth** limiting factors.



# Concept (1/2) – The Linear Regime

- □ Lossy Photonic Coupler
  - Two identical waveguides (same phase constant  $\beta_0$ )
  - Top waveguide has saturable losses (non-linear).
  - Bottom waveguide is lossless (linear).
  - Two port configuration.
  - Length = Coupling length  $L_c$
- □ Linear Regime (without SA)
  - Super-modes  $\beta = \beta_0 j\frac{\alpha}{2} \pm \sqrt{|\kappa|^2 (\frac{\alpha}{2})^2}$  Exceptional Point at  $\frac{\alpha}{2|\kappa|} = 1$ .

  - When  $\alpha/2|\kappa| > 1$  one supermode is lossy and the other is lossless (asymptotically).
  - The lossy supermode vanishes very fast: Light remains in the lossless waveguide.





# Concept (2/2) – The Non-linear (SA) Regime

$$\alpha \rightarrow \frac{\alpha}{1+|A_1|^2/|A_{\rm sat}|^2}$$

Assume that for  $|A_1| \ll |A_{sat}| \rightarrow \frac{\alpha}{2|\kappa|} \gg 1$ and half-duplex operation.



- □ High-power excitation from the lossy (SA) waveguide:
  - High overlap with the non-linear waveguide.
  - Due to SA:  $\alpha \to 0$ ,  $\alpha/2|\kappa| < 1$ . **Below EP**.
  - Light can couple to opposite waveguide (forward).





### Concept (2/2) – The Non-linear (SA) Regime

$$\alpha \rightarrow \frac{\alpha}{1 + |A_1|^2/|A_{\text{sat}}|^2}$$

Assume that for  $|A_1| \ll |A_{sat}| \rightarrow \frac{\alpha}{2|\kappa|} \gg 1$ and half-duplex operation.



□ High-power excitation **from the lossless waveguide**:

- Little overlap with the non-linear waveguide
- Losses are **not saturated**,  $\alpha/2|\kappa| \gg 1$ . **Above EP**.
- Light cannot couple to opposite waveguide (backward).





#### Concept Results – Coupled Mode Theory





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#### Concept Results – Coupled Mode Theory

#### **Conclusions from concept model:**

- ✓ Increasing  $a/2|\kappa|$  increases NRIR but also increases NL threshold
  - Higher losses are better!
  - Small  $|\kappa|$  leads to large devices
- Ideal performance (high transmission and/or perfect isolation) is inherently prohibited
  - A compromise must be made:
  - Narrow NRIR or high NL threshold
- At low and at very high powers the device is again reciprocal





#### Physical implementation with graphene (1/3)

#### □ Graphene monolayer characteristics at 1550 nm

- Linear conductivity  $\sigma_1 = \sigma_{intra} + \sigma_{inter}$ .
- Saturation of the **interband conductivity**.
- $|\mu_c| < 0.4 \text{ eV}$ , ideally totally saturable.
- SA has lower power threshold than other







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# Physical implementation with graphene (3/3)

- □ Pair of identical **silicon slot waveguides**.
  - Left waveguide overlaid with two graphene monolayers
  - Graphene is **unbiased**  $\mu_c = 0 \text{ eV}$ , so that  $\sigma \approx \sigma_{\text{inter}} \approx 122 \text{ }\mu\text{S}$
- □ The dimensions chosen ensure that:
  - Field is mainly guided in the slot area: high confinement.
  - TE polarization parallel to graphene: high interaction.



- □ Waveguide dimensions:
  - Height = 180 nm
  - Width = 360 nm
  - Slot = 40 nm
  - Gap = 640 nm
- □ Parameters
  - Coupling length  $L_c = 0.5\pi/|\kappa| = 800 \ \mu m$
  - Unsaturated losses  $\alpha = 0.42 \text{ dB}/\mu\text{m}$



CMT parameter

 $\alpha/2|\kappa| \approx 12$ 

$$\frac{\partial A_1}{\partial z} = \alpha_{\text{sat},1} (|A_1|^2) A_1 + \alpha_{\text{nsat},1} A_1 + i\kappa A_2,$$
$$\frac{\partial A_2}{\partial z} = \alpha_{\text{nsat},2} A_2 + i\kappa A_1,$$

- Graphene saturation intensity  $I_{sat} = 1 \text{ MW/cm}^2$
- Non-saturable losses  $a_{nsat,i} = 0$
- Coupling coefficient  $\kappa = \pi/2L_c$
- Normalization constant N<sub>i</sub>
  - Each equation is derived for a specific waveguide/mode (uncoupled) and then coupled heuristically
  - Approximation stands due to weak coupling





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$$\frac{\partial A_2}{\partial z} = \alpha_{\text{nsat},2} A_2 + i\kappa A_1, \qquad +i\gamma_s |A_1|^2 A_1$$

• Graphene saturation intensity 
$$I_{sat} = 1 \text{ MW/cm}^2$$

- Non-saturable losses  $a_{nsat,i} = 0$
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# Validating coupled NLSE

#### **Beam Propagation Method** (BPM)

Numerical step-wise propagation of an input excitation along a slowly varying waveguide

- ✓ Frequency-domain (CW) method
- Cross-section (xy plane): Hybrid higher-order vector/nodal finite-elements (FEM)
- ✓ z-propagation: Finite-difference Crank-Nicolson stepping scheme

#### **Non-linear BPM**

- Material EM properties (n for bulk materials and σ for sheet materials) depend on E-field intensity
- Graphene SA:  $\Delta \sigma(x, y, z) = -\sigma_{1,inter}(x, y) \cdot I_n/(1 + I_n)$ • Normalized intensity:  $I_n = \left|\vec{E}_{||}(x, y, z)\right|^2/(2Z_0 I_{sat})$
- In-step iterations for stability (2-3 are enough)



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#### Excellent agreement (0.2 dB) w/ NLSE





## Summary and Conclusions

#### To summarize:

□ Studied the **breaking of reciprocity** by utilizing EPs and SA.

Proposed a physical implementation using a silicon slot waveguide (SOI platform) and graphene

# 2 graphene layers (at $\mu_c \sim 0 \text{ eV}$ ) $\xrightarrow{\text{TE}}$ Air Si SiO<sub>2</sub> $\xrightarrow{\text{gap}}$ slot $L_c \xrightarrow{} L_c$ $\xrightarrow{} Z_1 \xrightarrow{g_2} -10$ $\xrightarrow{} NRIR$

#### **Conclusions:**

- □ SA combined with EPs as an alternative to the Kerr effect.
  - Lower power threshold than the Kerr effect.
  - Compatible with standard integration techniques.
  - Bandwidth is limited mainly by waveguide coupling!





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